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**Unit** : II  
**Topic** : Feedback Amplifier and  
Oscillators

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## UNIT – I

### Feedback Amplifier and Oscillators

- 1.1 Feedback:** Feedback is a technique in which, a part of output is sampled and feeding back to the input of the amplifier.

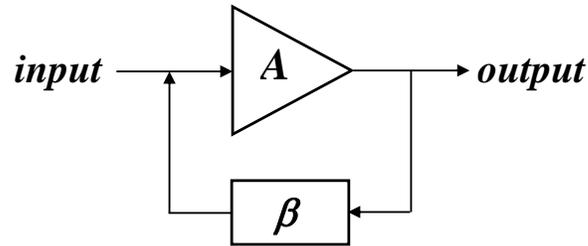


Figure 1.1: Feedback Circuit

- 1.2 Types of feedback:** Basically there are two types of feedback

- (i) Positive feedback
- (ii) Negative feedback

**Positive feedback:** When input signal and part of output signal are in phase (additive), the feedback is called **Positive or Regenerative** feedback. Positive feedback is used in the design of oscillators.

**Negative feedback:** When input signal and part of output signal are out of phase (subtractive), the feedback is called **Negative or Degenerative** feedback. Negative feedback is used in the design of amplifiers.

- 1.3 Gain of Negative Feedback Amplifier:**

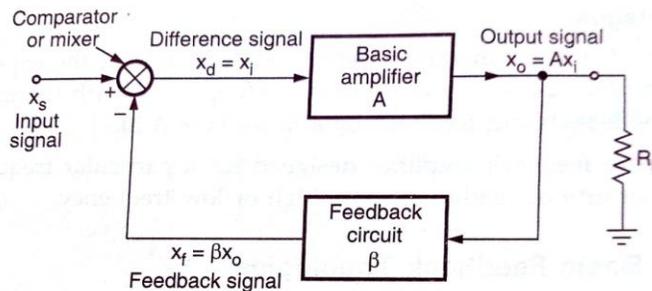


Figure 1.2: Negative Feedback Amplifier

From circuit gain of basic amplifier is given by

$$A = \frac{X_o}{X_i} \quad (i)$$

Gain of feedback network is given by

$$\beta = \frac{X_f}{X_o} \quad (ii)$$

Overall gain of feedback amplifier is given by

$$A_f = \frac{X_o}{X_s} \quad (iii)$$

The input signal is given by

$$X_i = X_s - X_f \quad (iv)$$

Or  $X_s = X_i + X_f = X_i + \beta X_o$

$$X_s = X_i + A \beta X_i = X_i (1 + A \beta) \quad (v)$$

Hence from equation (i) and (v)

$$A_f = \frac{X_o}{X_s} = \frac{AX_i}{X_i(1+A\beta)} \quad (vi)$$

Overall gain of negative feedback amplifier is given by

$$A_f = \frac{A}{1+A\beta} \quad (vii)$$

The equation shows that in **negative** feedback overall gain is decreased, hence it is also called **degenerative** feedback.

Overall gain of positive feedback amplifier is given by

$$A_f = \frac{A}{1-A\beta} \quad (viii)$$

The equation shows that in **positive** feedback overall gain is increased, hence it is also called **regenerative** feedback.

**1.4 Performance of Negative Feedback:** We have seen that gain of an amplifier is reduced when negative feedback is used. This is very serious drawback. But negative feedback improves the performance of the amplifier from so many other points. The reduction of gain due to negative feedback can always be compensated by increasing the number stages.

**1.5 Advantage of Negative feedback:**

- (i) It Improves the Stability of amplifier gain.
- (ii) It reduce the Distortion and Noise
- (iii) It increase the Input Impedance
- (iv) It decrease the Output Impedance
- (v) It Increase the Bandwidth

**1.5.1 Stabilization of Gain:** The gain of an amplifier may changes because of so many reasons. Change in power supply voltage. Change in parameter of active device (Transistors). If the gain of the amplifier was independent of these change. Negative feedback achieves this object to great extent.

The gain of negative feedback is given by:-

$$A_f = \frac{A}{1+A\beta}$$

If  $A\beta \gg 1$

Then 
$$A_f = \frac{A}{A\beta} = \frac{1}{\beta}$$

Thus, the gain  $A_f$  of the feedback amplifier is made independent of the internal gain  $A$ . The gain  $A_f$  depends only on  $\beta$ , Which in turn depends on passive elements such as resistors.

If a certain changes in the internal gain of the amplifier takes place. We can find corresponding percentage change in the overall gain of the feedback amplifier.

The gain of negative feedback is given by

$$A_f = \frac{A}{1 + A\beta}$$

Differentiating with respect to  $A$

$$\frac{dA_f}{dA} = \frac{(1+A\beta) \times 1 - A \times \beta}{(1+A\beta)^2} = \frac{1}{(1+A\beta)^2}$$

$$dA_f = \frac{dA}{(1+A\beta)^2}$$

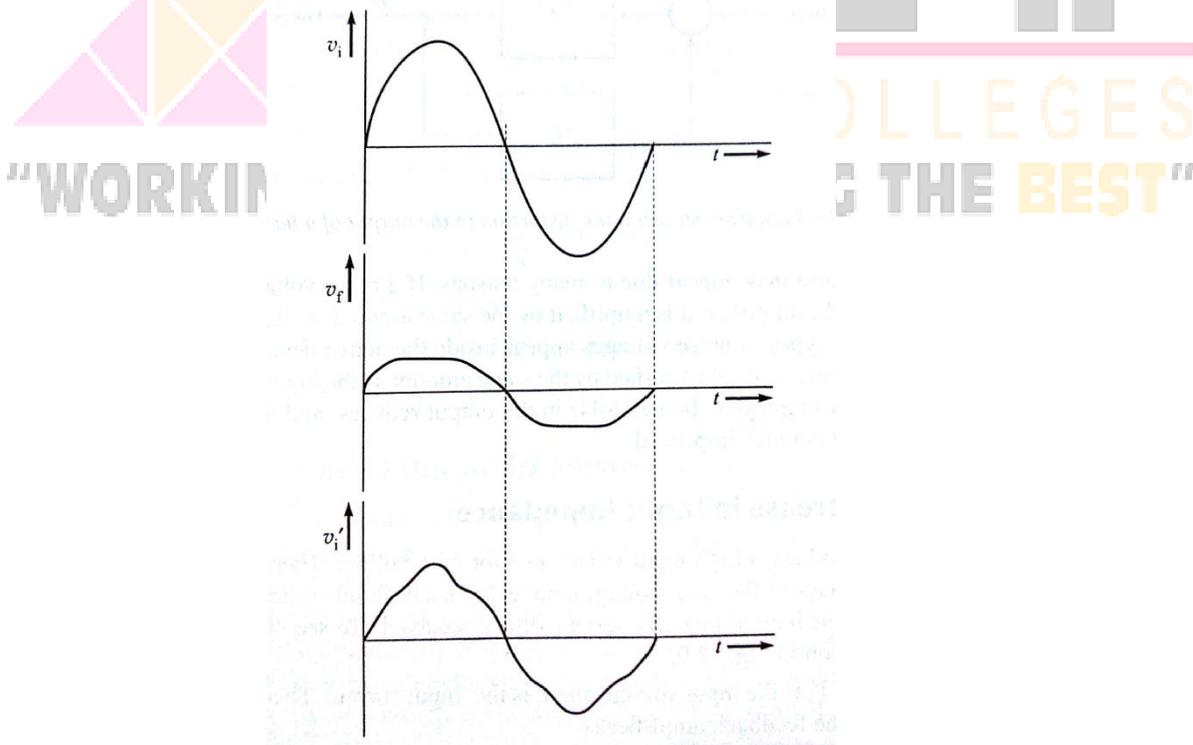
Dividing the above equation by  $A_f$

$$\frac{dA_f}{A_f} = \frac{dA}{(1+A\beta)^2} \times \frac{(1+A\beta)}{A}$$

Or 
$$\frac{dA_f}{A_f} = \frac{1}{(1+A\beta)} \left( \frac{dA}{A} \right)$$

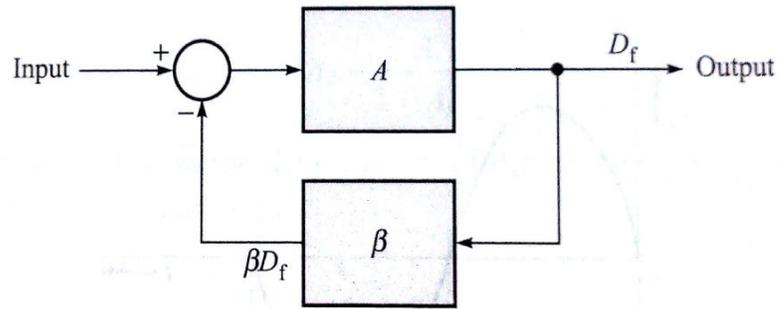
Since  $(1+A\beta) > 1$ , the percentage change in  $A_f$  is seen to be much less than the percentage change in  $A$ .

### 1.5.2 Reduction in Distortion and Noise:



**Figure 1.3: Distortion in amplifier**

As shown in figure 1.3 basic amplifier is assumed to be distort the sinusoidal input waveform by flattening the peaks. The feedback voltage  $V_f$  has the same waveform as the output waveform. The voltage  $V_f$  gets subtracted from the input voltage  $V_i$  to make the net output.



**Figure1.4: Reduction in Distortion**

As shown in figure 1.4 suppose the amplifier with gain  $A$  produces a distortion  $D$  without feedback. This distortion appears at the output. After feedback is applied, the gain becomes  $A_f$  and the distortion in the output becomes  $D_f$ . A part  $\beta D_f$  of the distortion  $D_f$  is feedback to the input. This gets amplified  $A$  times by the basic amplifier and becomes  $A\beta D_f$ . This gets added up (in reverse polarity) to the original distortion  $D$  to make the net distortion  $D_f$ .

$$D_f = D - A\beta D_f$$

$$D_f = \frac{D}{1+A\beta}$$

Thus we can see that the Distortion is reduced by the factor  $(1+A\beta)$ .

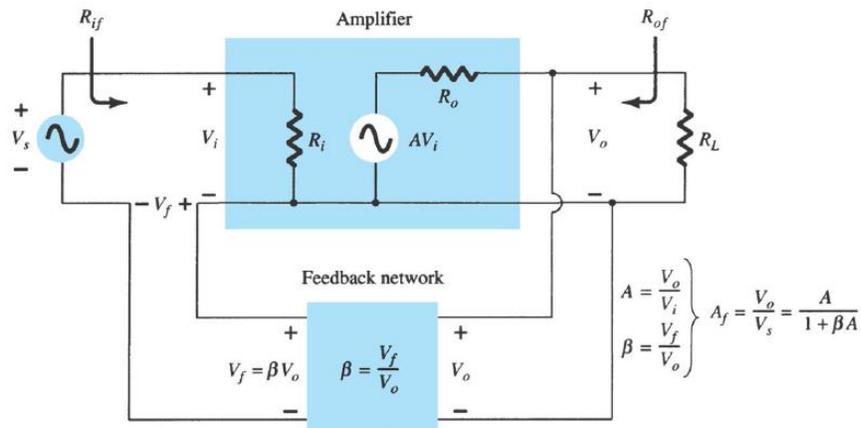
### 1.5.3 Increase in Input Impedance:

High input impedance reduces the loading effect. As shown in figure 1.5 input Resistance with feedback is given by:-

$$R_{if} = \frac{V_s}{I_i}$$

Where  $V_s = V_i + V_f$

$$= I_i R_i + \beta V_o = I_i R_i + A \beta V_i$$



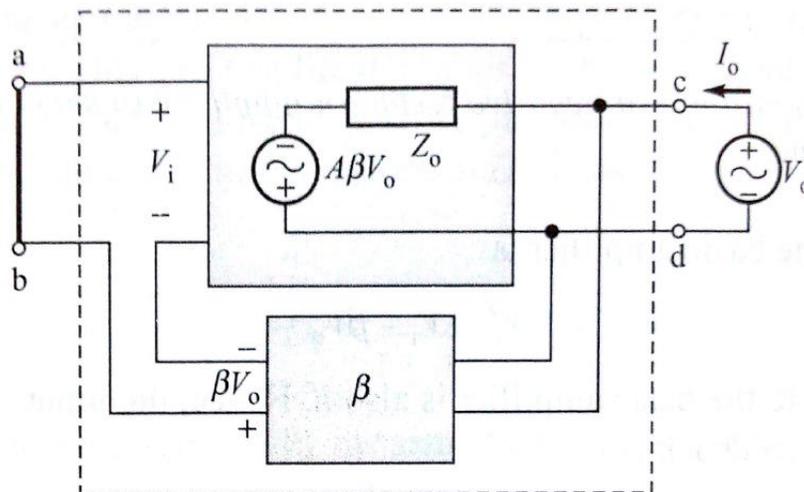
**Figure1.5: Input resistance with feedback**

$$V_s = I_i R_i + A \beta I_i R_i$$

$$R_{if} = \frac{V_s}{I_i} = R_i (1 + A\beta)$$

Thus we can see that the Input impedance increased by the factor  $(1+A\beta)$ .

### 1.5.4 Decrease in Output Impedance:



**Figure1.6: Output resistance with feedback**

Low output resistance is useful for impedance matching with load. As shown in figure 1.6 source voltage is removed and output is replaced with equivalent voltage source  $V_o$ . Output resistance with feedback is given by:-

$$Z_{of} = \frac{V_o}{I_o}$$

Applying KVL in output loop

$$V_o + A\beta V_o = I_o Z_o$$

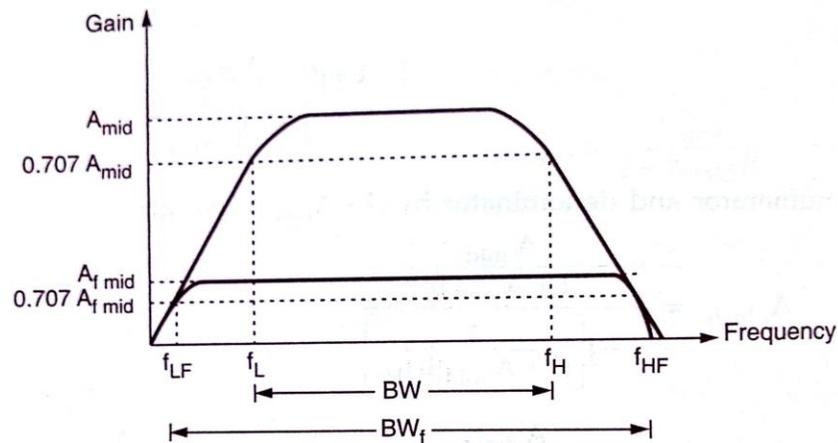
$$V_o(1 + A\beta) = I_o Z_o$$

Which gives

$$Z_{of} = \frac{Z_o}{1 + A\beta}$$

Thus we can see that the output impedance reduced by the factor  $(1 + A\beta)$ .

### 1.5.5 Increase in Bandwidth



**Figure1.7: Increase in Bandwidth**

As we know that introduction of negative feedback in an amplifier reduces its gain by  $(1 + A\beta)$ . But for an amplifier Gain Bandwidth Product (GBW) is always constant.

Let bandwidth of basic amplifier is  $BW$  and it is with negative feedback is  $BW_f$ . From the property of an amplifier

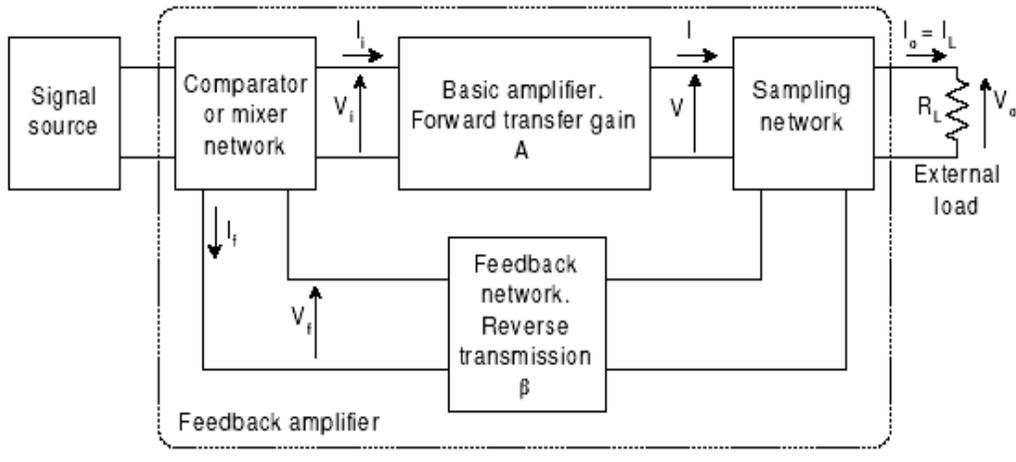
$$ABW = A_f BW_f$$

$$BW_f = \frac{A \times BW}{A_f} = \frac{A \times BW(1 + A\beta)}{A}$$

$$BW_f = BW(1 + A\beta)$$

Thus we can see that the Bandwidth increased by the factor  $(1 + A\beta)$ .

## 1.6 Feedback Amplifier



**Figure1.8: Feedback amplifier**

As shown in figure 1.8, block diagram of feedback amplifier has four important circuits,

- (i) Sampling Network
- (ii) Mixing Network
- (iii) Feedback Network and
- (iv) Basic Amplifier

### 1.6.1 Sampling Network:



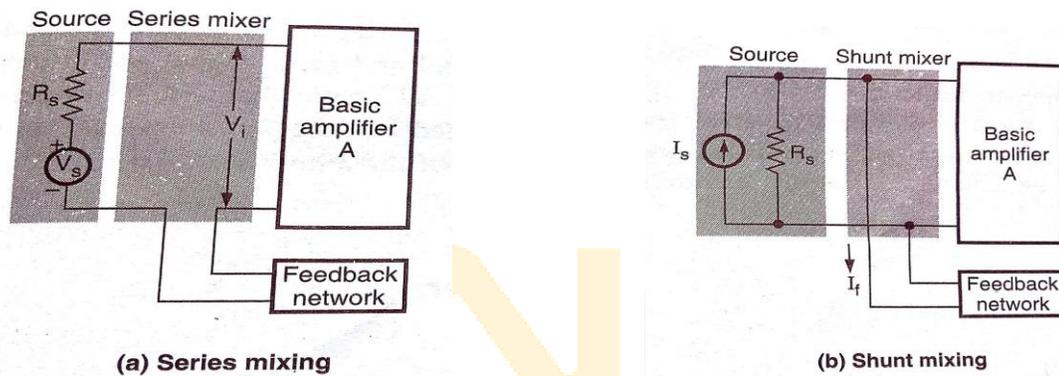
**Figure1.9: Sampling Networks**

There are two ways to sample the output, according to the sampling parameter, either current or voltage.

When the output voltage is sampled by connecting the feedback network in shunt across the output (Fig. 1.9a). This type of connection is referred to as **voltage or node sampling**.

When the output current is sampled by connecting the feedback network in series with the output (Fig.1.9b). This type of connection is referred to as **current or loop sampling**.

### 1.6.2 Mixing Network:



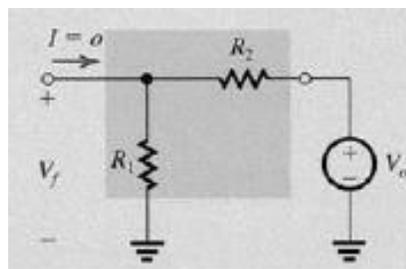
**Figure1.10: Mixing Networks**

There are two ways of mixing feedback signal with the input signal. These are Series mixing and Shunt mixing.

When the feedback signal is connected serially with input signal. This type of mixing is called **series mixing** (fig. 1.10a).

When the feedback signal is connected in parallel with input signal. This type of mixing is called **shunt mixing** (fig. 1.10b).

### 1.6.3 Feedback Network:



**Figure1.11: Feedback Network**

Feedback network is passive network as shown in figure 1.11. Input to the feedback network is output voltage of amplifier ( $V_o$ ), and output of feedback network is feedback voltage ( $V_f$ ) The feedback factor is represented by  $\beta$  and it is given by:-

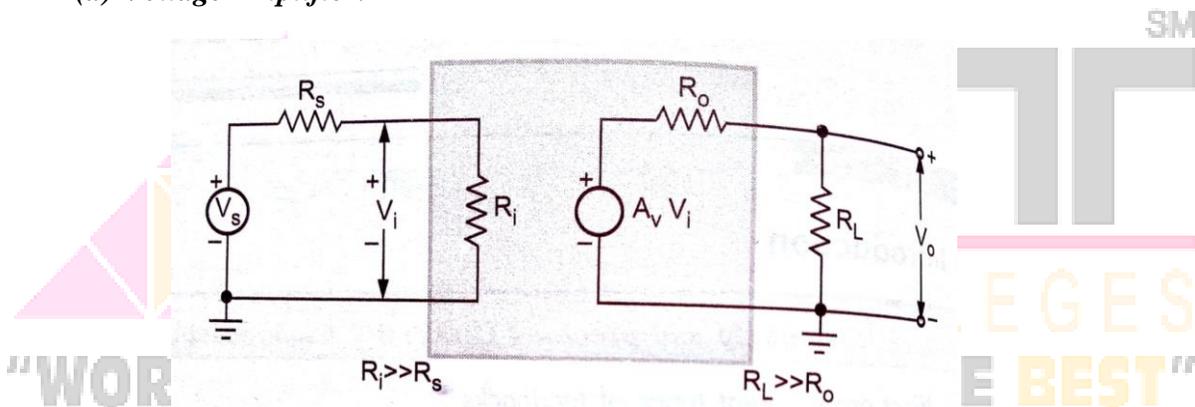
$$\beta = \frac{V_f}{V_o} = \frac{R_1}{R_1 + R_2}$$

#### 1.6.4 Basic Amplifier:

To fulfill the requirement Sampling and Mixing network, there are four type of amplifier

- (a) Voltage amplifier
- (b) Current amplifier
- (c) Trans-conductance amplifier and
- (d) Trans-resistance amplifier

(a) **Voltage Amplifier:**



**Figure1.12: Voltage Amplifier**

As shown in figure 1.12

if  $R_i \gg R_s, \quad V_i = V_s$

And if  $R_o \ll R_L,$

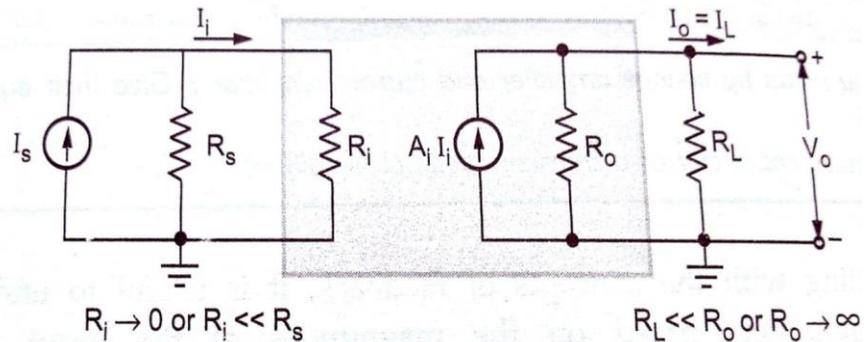
$$V_o = A_v V_i = A_v V_s$$

The Gain of Amplifier is

$$A_v = \frac{V_o}{V_s}$$

Hence **Voltage Amplifier** provides voltage output ( $V_o$ ) proportional to the signal or source voltage ( $V_s$ ).

**(b) Current amplifier**



**Figure 1.13: Current Amplifier**

As shown in figure

if  $R_i \ll R_s, \quad I_i = I_s$

And if  $R_o \gg R_L,$

$$I_o = A_i I_i = A_i I_s$$

The Gain of Amplifier is

$$A_i = \frac{I_o}{I_s}$$

Hence **Current Amplifier** provides current output ( $I_o$ ) proportional to the signal or source current ( $I_s$ ).

**(c) Trans-conductance amplifier**

As shown in figure 1.13

if  $R_i \gg R_s, \quad V_i = V_s$

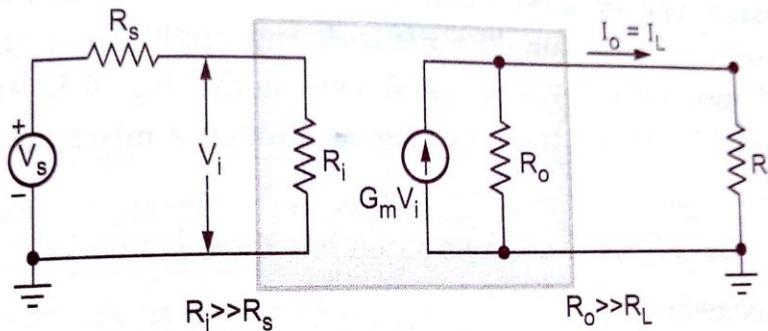
And if  $R_o \gg R_L,$

$$I_o = G_m V_i = G_m V_s$$

The Gain of Amplifier is given as

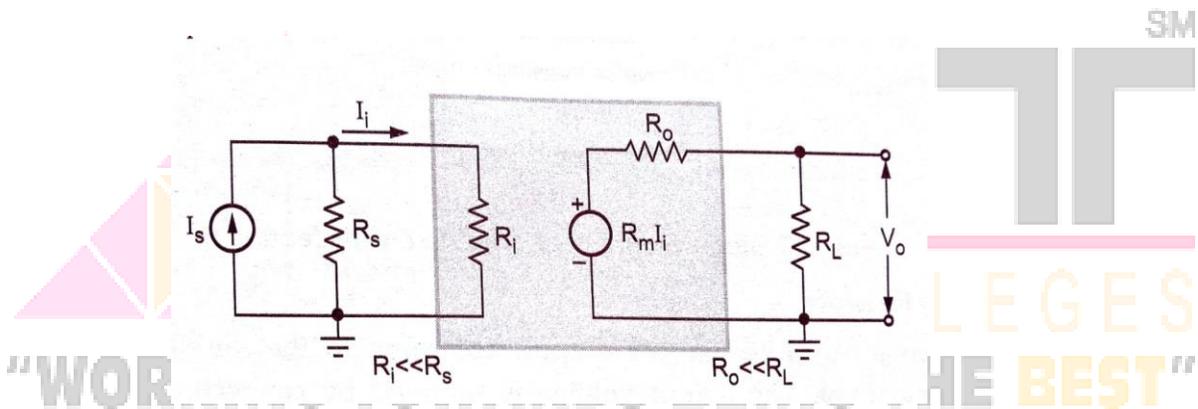
$$G_m = \frac{I_o}{V_s}$$

Hence **Trans-conductance** Amplifier provides current output ( $I_o$ ) that is proportional to the signal or source voltage ( $V_s$ ).



**Figure1.13: Trans-conductance amplifier**

(d) *Trans-resistance amplifier*



**Figure1.14: Trans-resistance amplifier**

As shown in figure 1.14

if  $R_i \ll R_s$ ,  $I_i = I_s$

And if  $R_o \ll R_L$ ,

$$V_o = R_m I_i = R_m I_s$$

The Gain of Amplifier is

$$R_m = \frac{V_o}{I_s}$$

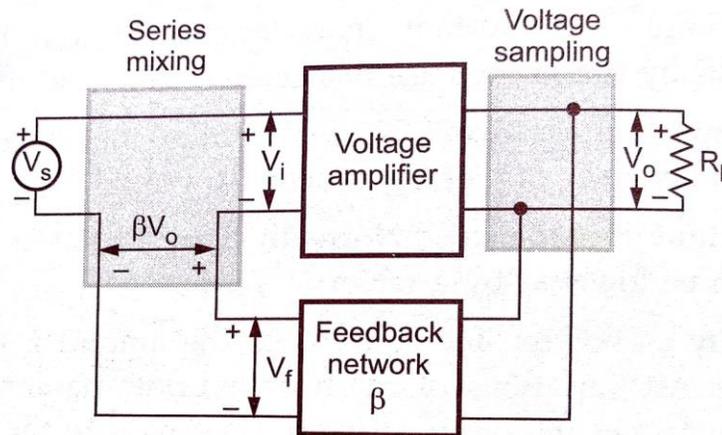
Hence **Trans-resistance** Amplifier provides voltage output ( $V_o$ ) that is proportional to the signal or source current ( $I_s$ ).

## 1.6 Feedback Topology

Sampling and mixing network in addition with four basic amplifier gives four feedback topologies.

- (i) Voltage – Series feedback Topology
- (ii) Current - Series feedback Topology
- (iii) Voltage – Shunt feedback Topology
- (iv) Current – Shunt feedback Topology

### 1.6.1 Voltage – Series feedback Topology



**Figure 1.15: Voltage – Series feedback Topology**

As shown in figure 1.15, input to the feedback network is parallel with the output of the amplifier. A fraction of output voltage through feedback network is applied in series with the input voltage of the amplifier. The series connection at the input increase the input resistance and parallel connection at the output decrease the output resistance. In this topology amplifier used is voltage amplifier, its gain is given by

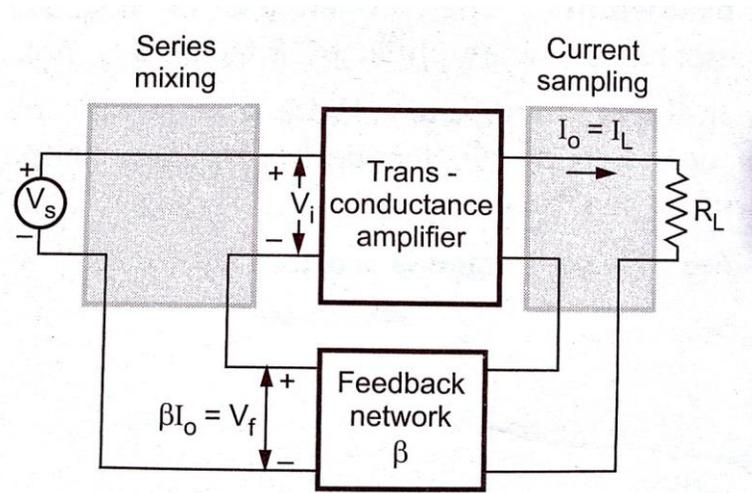
$$A_v = \frac{V_o}{V_s}$$

And the feedback factor is given by

$$\beta = \frac{V_f}{V_o}$$

### 1.6.2 Current - Series feedback Topology

As shown in figure 1.16, input to the feedback network is in series with the output of the amplifier. A fraction of output current through feedback network is applied in series with the input voltage of the amplifier. The series connections at the input and at the output increase the input and output resistances.



**Figure1.15: Current - Series feedback Topology**

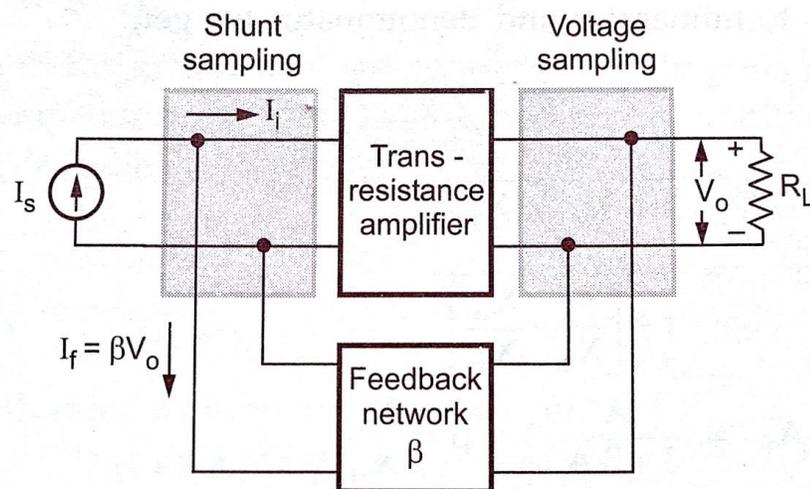
In this topology, amplifier used is trans-conductance amplifier; its gain is given by

$$G_m = \frac{I_o}{V_s}$$

And the feedback factor is given by

$$\beta = \frac{V_f}{I_o}$$

### 1.6.3 Voltage – Shunt feedback Topology



**Figure1.16: Voltage – Shunt feedback Topology**

As shown in figure 1.16, input to the feedback network is parallel with the output of the amplifier. A fraction of output voltage through feedback network is applied in parallel with the input current of the amplifier. The shunt connection at the input and output reduces the input and output resistance.

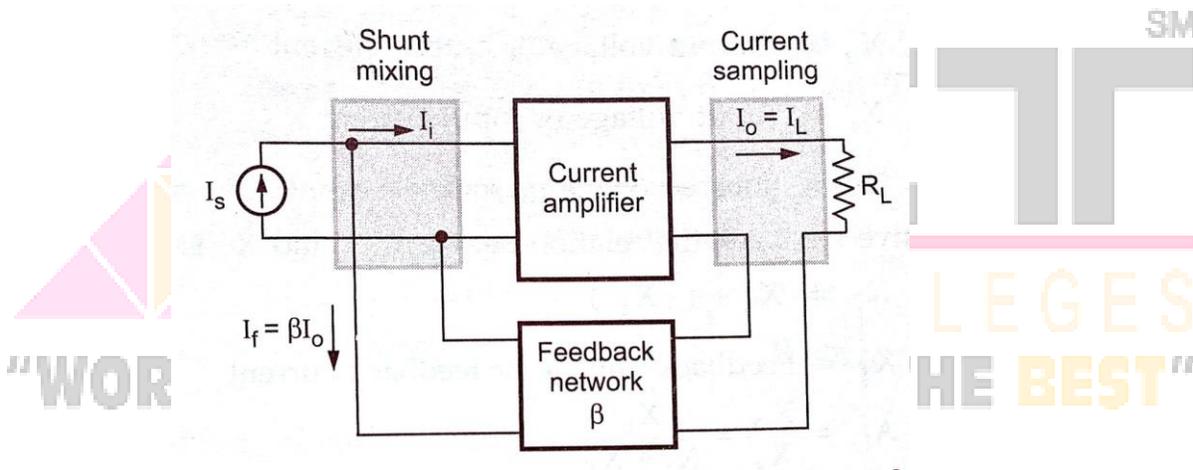
In this topology, amplifier used is trans-resistance amplifier its gain is given by

$$R_m = \frac{V_o}{I_s}$$

And the feedback factor is

$$\beta = \frac{I_f}{V_o}$$

### 1.6.3 Current – Shunt feedback Topology



**Figure1.17: Current – Shunt feedback Topology**

As shown in figure 1.17, input to the feedback network is in series with the output of the amplifier. A fraction of output current through feedback network is applied in parallel with the input current of the amplifier. The shunt connection at the input reduces the input resistance and the series connection at the output increase the output resistance.

In this topology, amplifier used is current amplifier its gain is given by

$$A_i = \frac{I_o}{I_s}$$

And the feedback factor is  $\beta = \frac{I_f}{I_o}$

## 1.7 Comparison Between various Feedback Topology

Characteristics	Voltage – Series	Current – Series	Voltage – Shunt	Current - Shunt
<b>Voltage Gain</b>	Decrease	Decrease	Decrease	Decrease
<b>Distortion</b>	Decrease	Decrease	Decrease	Decrease
<b>Bandwidth</b>	Increase	Increase	Increase	Increase
<b><math>R_{if}</math></b>	Increase	Increase	Decrease	Decrease
<b><math>R_{of}</math></b>	Decrease	Increase	Decrease	Increase

### Tutorials

1. An amplifier with negative feedback has a voltage gain 100. It is found that without feedback, an input signal of 50mV is required to produce a given output; whereas with feedback, the signal must be 0.6V for the same output. Calculate the value of A and  $\beta$ .  
(1200, 0.916%)
2. To an amplifier of 60dB gain, a negative feedback of 0.005 is applied. What would be the change in overall gain of the feedback amplifier if the internal amplifier is subjected to a gain of 12%?  
(2%)
3. We have an amplifier of 60dB gain. It has an output impedance  $Z_o=12K\Omega$ . It is required to modify its output impedance to  $600\Omega$  by applying negative feedback. Calculate the value of feedback factor. Also find the performance change in the overall gain, for 10% change in the gain of the internal amplifier.  
(1.9%, 0.5)
4. An Amplifier has a midband gain of 125 and a bandwidth of 250kHz. (a) If 4% feedback is introduced, find the new bandwidth and gain. (b) If the bandwidth is restricted to 1MHz, find the feedback ratio.  
(1.5MHz, 20.83, 2.4%)
5. A voltage series negative feedback amplifier has a voltage gain without feedback of  $A=500$ , input resistance  $R_i=3k\Omega$ , output resistance  $R_o=20k\Omega$  and feedback ratio  $\beta=0.01$ .

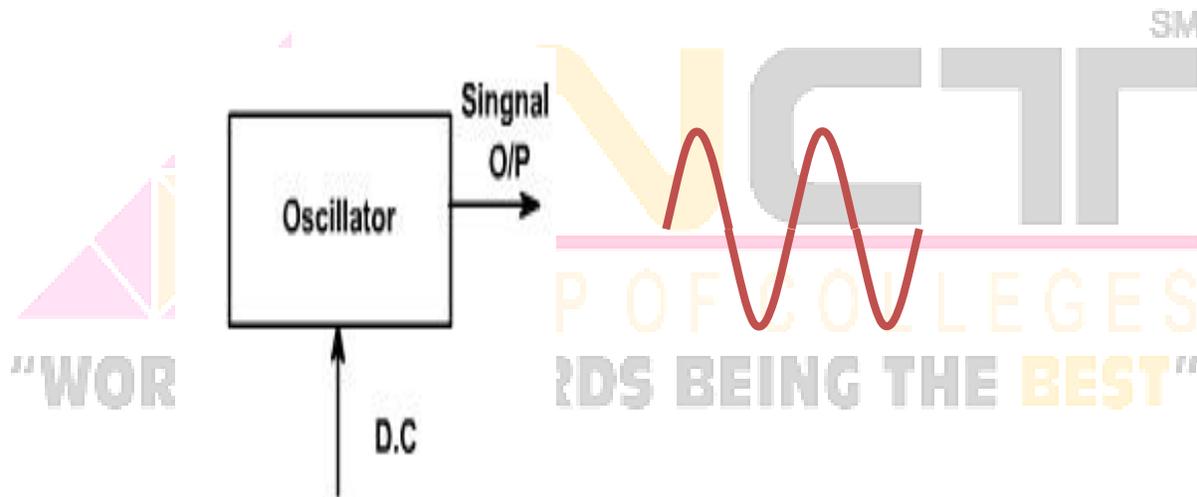
Calculate the voltage gain  $A_f$ , input resistance  $R_{if}$ , and output resistance  $R_{of}$  of the amplifier with feedback. **(83.33, 18k, 3.33k)**

- The distortion in an amplifier is found to be 3%, when the feedback ratio of negative feedback amplifier is 0.04. When the feedback is removed, the distortion becomes 15%. Find the open loop and closed loop gain. **(100, 20)**
- An amplifier with open loop gain of  $A=2000\pm 150$  is available. It is necessary to have the amplifier whose voltage gain varies by not more than  $\pm 0.2\%$ . Calculate  $\beta$  and  $A_f$ . **(1.825%, 53.33)**

## 1.8 Oscillator:

Any circuit that generates an alternating signal is called oscillator. To generate ac signal, the circuit is supplied energy from a dc source. The oscillators have variety of applications. In some application we need signal of low frequencies, in other of very high frequencies. For example, to test the performance of a stereo amplifier, we need an oscillator of variable frequency in audio range (20Hz – 20kHz), which is called audio frequency generator. Generation of high frequency is essential in all communication system. For example in radio and television broadcasting, the transmitter radiates the signal using a carrier of very high frequency. Some applications of communication system with their frequency band is given below.

550 kHz – 22 MHz	Radio broadcasting
88 MHz – 108 MHz	for FM radio
1 GHz – 4 GHz	for DTH, TV and satellite Communication



**Figure 1.18: Block diagram of Oscillator**

Figure 1.18 shows that oscillator is an electronics source of alternating current or voltage having sine, square or saw tooth waves. Oscillator is a circuit which generates an *ac* source without requiring any externally applied input signal. It is a circuit which converts *dc* energy into *ac* energy at very high frequency.

## 1.9 Comparison between Amplifier and Oscillator:

Comparison between an amplifier and an oscillator is explained in table 2.

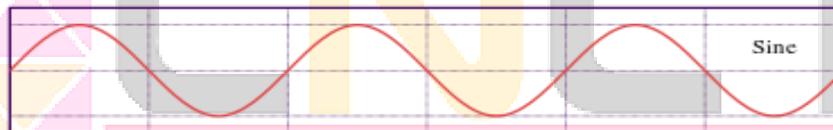
<b>Amplifier</b>	<b>Oscillator</b>
1. An amplifier produces an output signal whose waveform is similar to	1. An oscillator produce an output signal without any input signal

<p>input signal.</p> <ol style="list-style-type: none"> <li>2. Amplifier is an energy convertor; the process of energy conversion is controlled by the input signal.</li> <li>3. If there is no input signal, there is no energy conversion and hence there is no output.</li> </ol>	<ol style="list-style-type: none"> <li>2. Oscillator does not require an external signal to maintain energy conversion process.</li> <li>3. It keeps producing an output signal if the source is removed out.</li> <li>4. Frequency of the output signal is determined by the passive components used in the oscillator.</li> </ol>
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### 1.10 Classification of Oscillator:

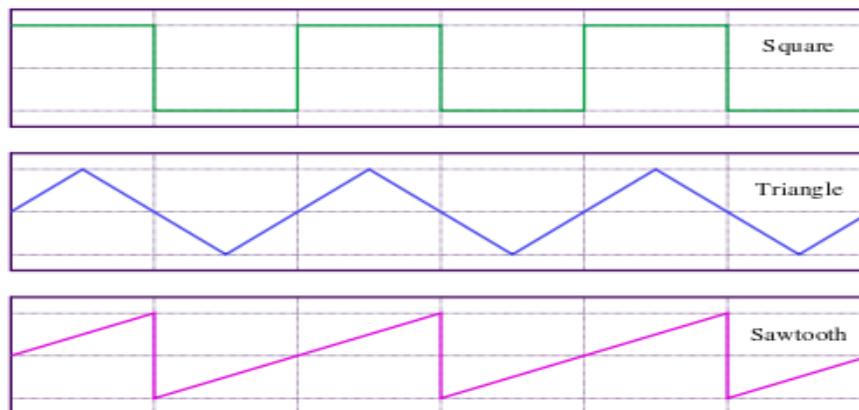
Electronic oscillator may be broadly divided into following two group:

- (i) **Sinusoidal or harmonic oscillator** which produce an output having sine waveforms as shown in figure 1.19.



**Figure 1.19 Sinusoidal wave**

- (ii) **Non-Sinusoidal or relaxation oscillator** they produce an output which has square, saw tooth, triangular waveforms etc.



**Figure 1.19 Non-Sinusoidal waves**

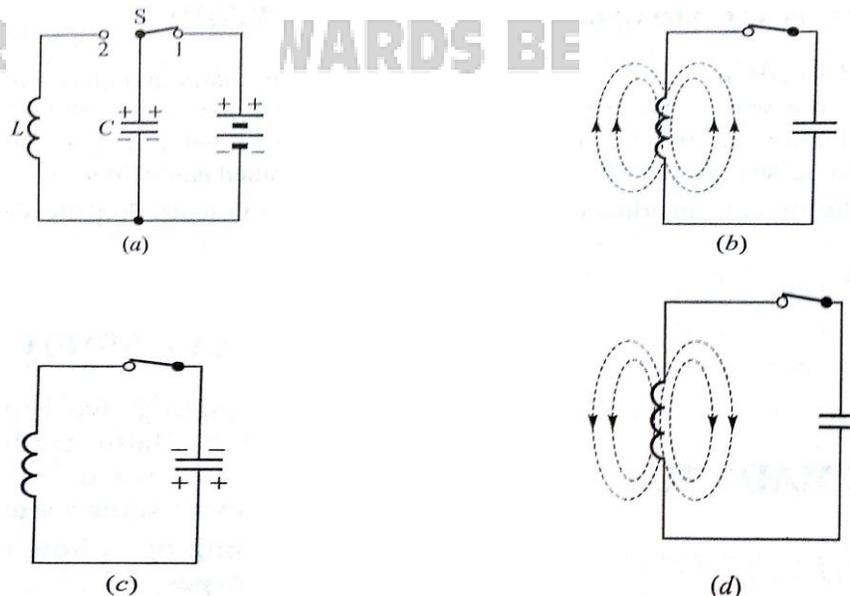
Oscillator may further classified based on their construction into following category:

- (i) Tuned circuits or LC oscillators such as Hartley, Colpitts and clapp oscillator.
- (ii) R-C oscillators such as R-C phase shift and Wien bridge oscillator.
- (iii) Negative resistance oscillators such as tunnel diode oscillator and UJT relaxation oscillator.
- (iv) Crystal oscillator.
- (v) Multivibrators such as astable, monostable and bistable multivibrator.

Oscillator may also be classified based on frequency of oscillation as:

- (i) Audio frequency oscillator : up to 20kHz.
- (ii) Radio frequency oscillator : 20kHz to 30MHz.
- (iii) Very high frequency oscillator : 30MHz to 300MHz
- (iv) Ultra high frequency oscillator : 300MHz to 3GHz
- (v) Microwave frequency oscillator : above 3GHz

### 1.11 Tank Circuit or Tuned Circuit:



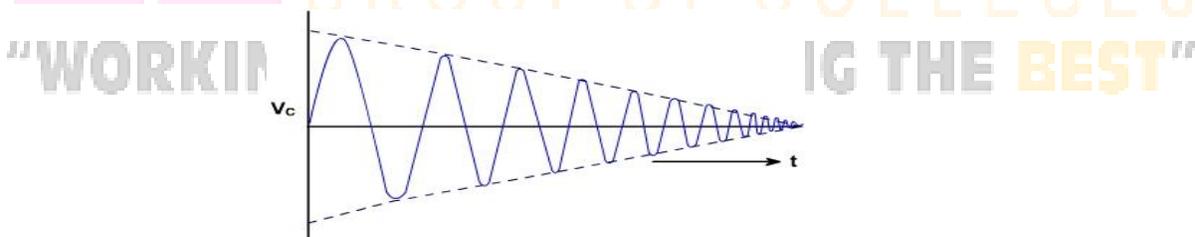
**Figure 1.20 Working of Tank Circuit**

Tank circuit is also known as frequency determining network, it is design with a capacitor and an inductor connected in parallel. As shown in fig. 1.20(a) energy is introduced into this circuit by connecting the capacitor to a DC voltage source. The capacitor is charged by DC source and there is a voltage across it. We say that energy is stored in the capacitor in the form of *electro-static energy*.

When the switch S is thrown to position 2, current start flowing in the circuit. The capacitor now starts discharging through inductor. Since the inductor has the property of opposing any change in current, the current build up slowly. Maximum current flows in the circuit when the capacitor is fully discharge. At this instant, electro-static energy is converted into *electro-magnetic energy* around the coil as shown in fig. 1.20(b).

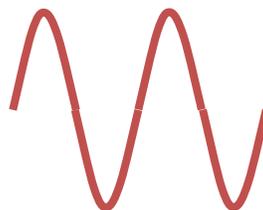
Once the capacitor is fully discharged, the magnetic field begins to collapse. The back emf in the inductor keeps the current flowing in the same direction. The capacitor starts charging, but with opposite polarity this time as shown in fig 1.20(c). As the charge builds up across the capacitor, the current decreases and the magnetic field decrease. Once again all the energy in the form of electro-static energy.

The capacitor now begins to discharge again. This time current flows in the opposite direction. Fig. 1.20(d) shows the capacitor fully discharged, and maximum current flowing in the circuit. Again all the energy is in form of electro-magnetic energy. The interchange of '*Oscillation*' of energy between *L* and *C* is repeated again and again. Since some energy is lost during interchange, the amplitude of each half cycle goes on decreasing. Hence we get *damped oscillation* as shown in figure 1.21.



**Figure 1.21 Damped Oscillations**

The oscillation of LC tank circuit can be maintained at a constant level. For this we have to supply a pulse of energy at the right time in each cycle. The resulting undamped oscillations are called *sustained oscillation*.



**Figure 1.21 Sustained Oscillations**

**1.11.1 Frequency of Oscillation:** Frequency of oscillation is also known as resonant frequency of tank circuit it can be determine as.

At resonance both inductive and capacitive reactance are equal.

$$X_L = X_C$$

$$2\pi f_o L = \frac{1}{2\pi f_o C}$$

$$f_o^2 = \frac{1}{4\pi LC}$$

It gives 
$$f_o = \frac{1}{2\pi\sqrt{LC}}$$

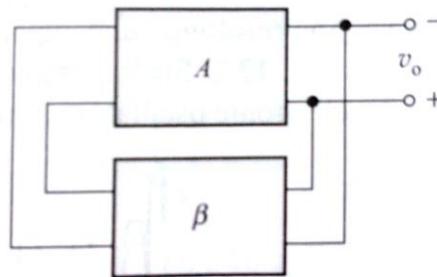
where

L – Inductance of inductor (in Henry)

C – Capacitance of capacitor (in Farad)

$f_o$  – Frequency of oscillation (in Hertz)

**1.11.2 Barkhausen Criterion:**



**Figure 1.22 Barkhusen Criterion**

An oscillator generates AC output signal without any input AC signal. A part of output is feedback to the input positively. This feedback signal is the only input to the internal amplifier. To find necessary condition for the sustained oscillations, positive feedback is required.

The overall gain of positive feedback amplifier is given by

$$A_f = \frac{V_o}{V_{in}} = \frac{A}{1-A\beta}$$

Since  $V_{in} = 0$

$$1 - A\beta = 0$$

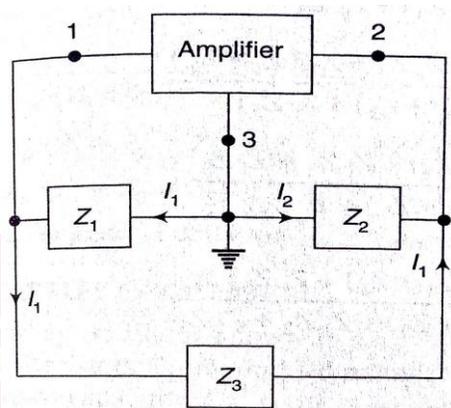
Or

$$A\beta = 1$$

Hence the essential conditions for maintaining oscillation are:

- (a) The magnitude of loop gain must be unity  $A\beta = 1$ .
- (b) The total phase shift around the closed loop is  $0^\circ$  or  $360^\circ$ .

### 1.12 General form of an Oscillator:



**Figure 1.23 General form of oscillator**

Figure 1.23 shows the general form of the oscillator. Any of the active devices such as Vacuum tube, Transistor, FET and Op-Amp may be used in the amplifier section.  $Z_1$ ,  $Z_2$  and  $Z_3$  are reactive elements constituting the feedback tank circuit, which determine the frequency of oscillation.

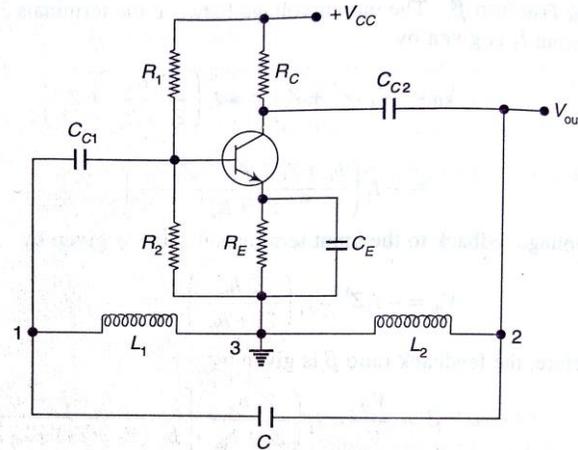
Frequency of oscillation of the LC oscillator is given by:

$$f_o = \frac{1}{2\pi\sqrt{LC}}$$

$Z_1$  and  $Z_2$  serves as voltage divider for output voltage and feedback signal. Therefore, the voltage across  $Z_1$  is the feedback signal. The feedback fraction is given by:

$$\beta = \frac{Z_1}{Z_2}$$

### 1.13 Hartley Oscillator



**Figure 1.24 Hartley oscillator**

### Construction

By comparing general form of oscillator with figure 1.24  $Z_1$  and  $Z_2$  are inductors and  $Z_3$  is a capacitor. Resistor  $R_1$ ,  $R_2$  and  $R_E$  provides necessary dc bias to the transistor.  $C_E$  is a bypass capacitor.  $C_{C1}$  and  $C_{C2}$  are coupling capacitors. The feedback network consisting of inductors  $L_1$ ,  $L_2$  and a capacitor  $C$  determines the frequency of oscillation.

### Working

When the supply voltage  $+V_{CC}$  is switched ON, a transient current is produced in tank circuit and consequently, damped oscillation are set up in the circuit. The oscillatory current in the tank circuit produces ac voltages across  $L_1$  and  $L_2$ . As terminal 3 is at ground potential, voltage developed at terminal 1 is positive and it is at terminal 2 is negative with respect to ground. Thus the phase difference between the terminal 1 and 2 is  $180^\circ$ . In the CE mode the transistor provides a phase difference of  $180^\circ$ . Therefore the total phase shift is  $360^\circ$ . Thus the necessary condition for sustained oscillation is satisfied. If the feedback is adjusted so that the loop gain  $A\beta = 1$ , the circuit acts as an oscillator.

The frequency of oscillation is given by:

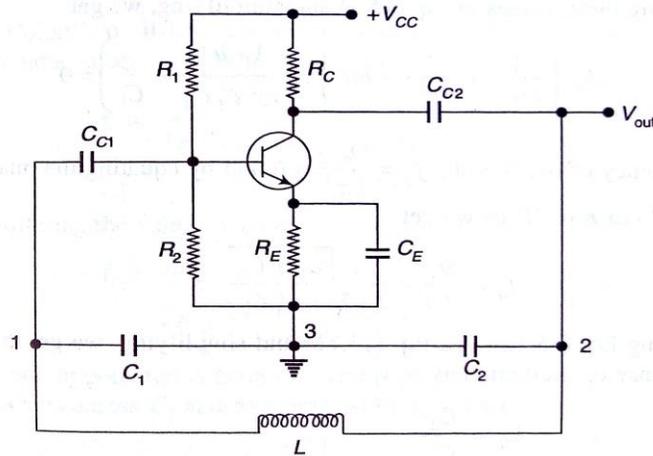
$$f_o = \frac{1}{2\pi\sqrt{L_{eq}C}}$$

where  $L_{eq} = L_1 + L_2$

Since the output voltage appears across  $L_2$  and the feedback voltage across  $L_1$ , the feedback fraction is given by:

$$\beta = \frac{Z_1}{Z_2} = \frac{X_{L1}}{X_{L2}} = \frac{L_1}{L_2}$$

## 1.14 Colpitts Oscillator



**Figure 1.25 Colpitts oscillator**

### Construction

By comparing general form of oscillator with figure 1.25  $Z_1$  and  $Z_2$  are capacitors and  $Z_3$  is an inductor. Resistor  $R_1$ ,  $R_2$  and  $R_E$  provides necessary dc bias to the transistor.  $C_E$  is a bypass capacitor.  $C_{C1}$  and  $C_{C2}$  are coupling capacitors. The feedback network consisting of capacitors  $C_1$ ,  $C_2$  and an inductor  $L$  determines the frequency of oscillation.

### Working

When the supply voltage  $+V_{CC}$  is switched ON, a transient current is produced in tank circuit and consequently, damped oscillation are set up in the circuit. The oscillatory current in the tank circuit produces ac voltages across  $C_1$  and  $C_2$ . As terminal 3 is at ground potential, voltage developed at terminal 1 is positive and it is at terminal 2 is negative with respect to ground. Thus the phase difference between the terminal 1 and 2 is  $180^\circ$ . In the CE mode the transistor provides a phase difference of  $180^\circ$ . Therefore the total phase shift is  $360^\circ$ . Thus the necessary condition for sustained oscillation is satisfied. If the feedback is adjusted so that the loop gain  $A\beta = 1$ , the circuit acts as an oscillator. Since the output voltage appears across  $C_2$  and the feedback voltage across  $C_1$ , the feedback fraction is given by

$$\beta = \frac{Z_1}{Z_2} = \frac{X_{C1}}{X_{C2}} = \frac{C_2}{C_1}$$

The frequency of oscillation is given by:

$$f_o = \frac{1}{2\pi\sqrt{LC_{eq}}}$$

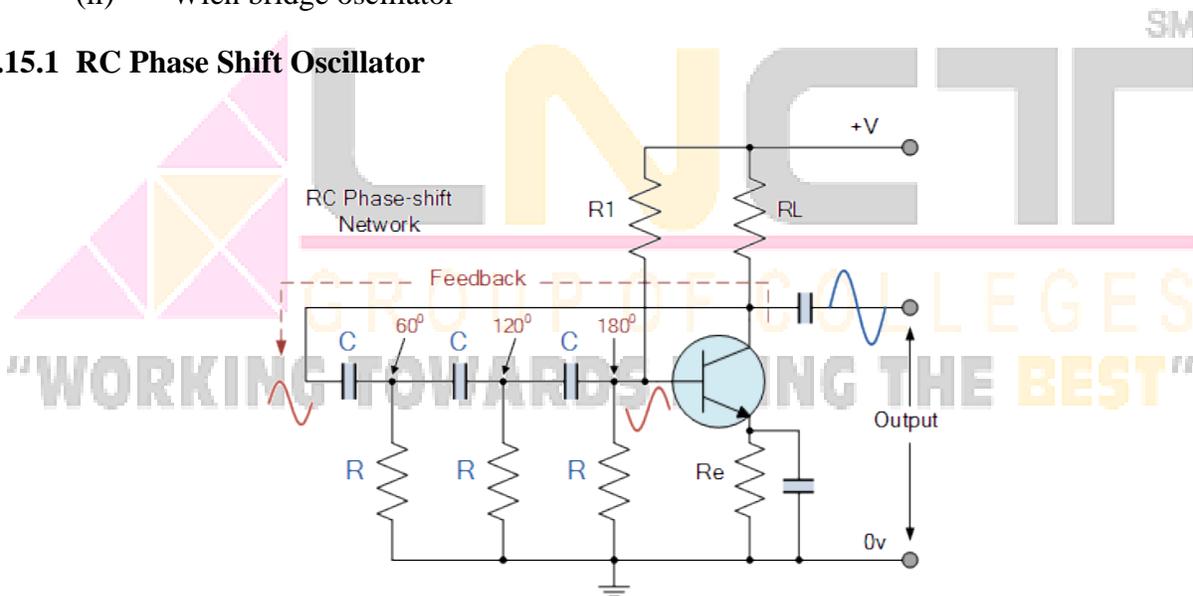
Where  $C_{eq} = \frac{C_1 C_2}{C_1 + C_2}$

## 1.15 RC Oscillators

All the oscillators using tuned LC circuit operates on high frequencies. At low frequency, inductors and capacitors required for the time circuit would be very bulky. RC oscillators found to be more suitable. Two important RC oscillators are:-

- (i) RC Phase shift oscillator and
- (ii) Wien bridge oscillator

### 1.15.1 RC Phase Shift Oscillator



**Figure 1.26 RC Phase Shift Oscillator**

In RC phase shift oscillator as shown in figure 1.26 the required phase shift of  $180^\circ$  in the feedback loop from output to input is obtained by using R and C components instead of tank circuit. As shown in figure RC phase shift oscillator uses cascade connection of high pass filter. This oscillator is designed by three RC section followed by a common emitter amplifier. The phase difference  $\Phi$  for each section is given by:

$$\phi = \tan^{-1} \left( \frac{1}{\omega CR} \right)$$

Each RC network provides a phase difference of  $\Phi$  which is between  $0 - 90^\circ$ . If R is adjusted such that  $\Phi$  becomes  $60^\circ$ . If the value of R and C are so chosen that, for the given frequency  $f_o$ , the phase shift of each RC section is  $60^\circ$ . Thus such a RC ladder network produces a total phase shift of  $180^\circ$  between the input and output voltage for given frequency. The other  $180^\circ$  phase shift is provided by transistor in common emitter mode. In this way the total phase shift in loop is  $360^\circ$  or  $0^\circ$ . Thereby satisfying the Barkhausen criterion for oscillation.

The frequency of oscillation is given by:

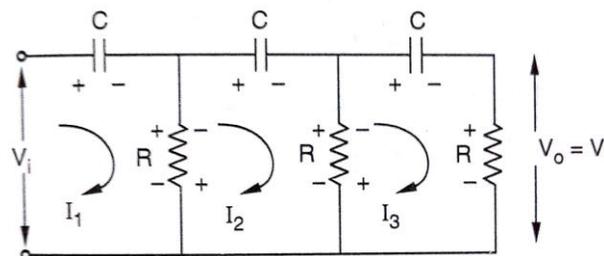
$$f_o = \frac{1}{2\pi RC\sqrt{6}}$$

At this frequency it is found that feedback factor of network is

$$|\beta| = \frac{1}{29}$$

In order that  $|\beta A|$  shall not be less than unity, it is require that the amplifier gain  $|A|$  must be more than 29 for sustained oscillation.

### Frequency of RC Phase Shift Oscillator



**Figure 1.26 RC Cascaded Network**

Applying KVL to various loops we get,

$$I_1 \left( R + \frac{1}{j\omega C} \right) - I_2 R = V_1$$

$$-I_1 R + I_2 \left( 2R + \frac{1}{j\omega C} \right) - I_3 R = 0$$

$$0 - I_2 R + I_3 \left( 2R + \frac{1}{j\omega C} \right) = 0$$

Replacing  $j\omega$  by  $s$  and writing the equations in matrix form,

$$\begin{bmatrix} R + \frac{1}{sC} & -R & 0 \\ -R & 2R + \frac{1}{sC} & -R \\ 0 & -R & 2R + \frac{1}{sC} \end{bmatrix} \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix} = \begin{bmatrix} V_i \\ 0 \\ 0 \end{bmatrix}$$

by applying Cramer's rule,  $I_3$  is given as

$$I_3 = \frac{V_i s^3 R^2 C^3}{1 + 5sRC + 6s^2 C^2 R^2 + s^3 C^3 R^3}$$

now

$$V_o = V_f = I_3 R = \frac{V_i s^3 R^3 C^3}{1 + 5sRC + 6s^2 C^2 R^2 + s^3 C^3 R^3}$$

Feedback factor is

$$\beta = \frac{V_f}{V_i} = \frac{s^3 R^3 C^3}{1 + 5sRC + 6s^2 C^2 R^2 + s^3 C^3 R^3}$$

Replacing  $s$  by  $j\omega$

$$\beta = \frac{-j\omega^3 R^3 C^3}{1 + 5j\omega RC - 6\omega^2 C^2 R^2 - j\omega^3 C^3 R^3}$$

Dividing numerator and denominator by  $-j\omega^3 R^3 C^3$  and replacing  $1/\omega RC$  by  $\alpha$  we get

$$\beta = \frac{1}{1 + 6j\alpha - 5\alpha^2 - j\alpha^3}$$

$$\beta = \frac{1}{(1 - 5\alpha^2) + j\alpha(6 - \alpha^2)}$$

To have phase shift of  $180^\circ$ , the imaginary part in the denominator must be zero.

hence  $\alpha(6 - \alpha^2) = 0$

Which gives  $\alpha^2 = 6$

Or  $\alpha = \sqrt{6}$

$$\frac{1}{\omega RC} = \sqrt{6}$$

$$\omega = \frac{1}{RC\sqrt{6}}$$

Thus the frequency of oscillation is

$$f_o = \frac{1}{2\pi RC\sqrt{6}}$$

$$\beta = \frac{1}{1 - 5 \times (\sqrt{6})^2} = -\frac{1}{29}$$

At this frequency

Or

$$|\beta| = \frac{1}{29}$$

Now to have oscillation  $|A\beta| \geq 1$

$$|A||\beta| \geq 1$$

$$|A| \geq \frac{1}{|\beta|} \geq \frac{1}{\frac{1}{29}}$$

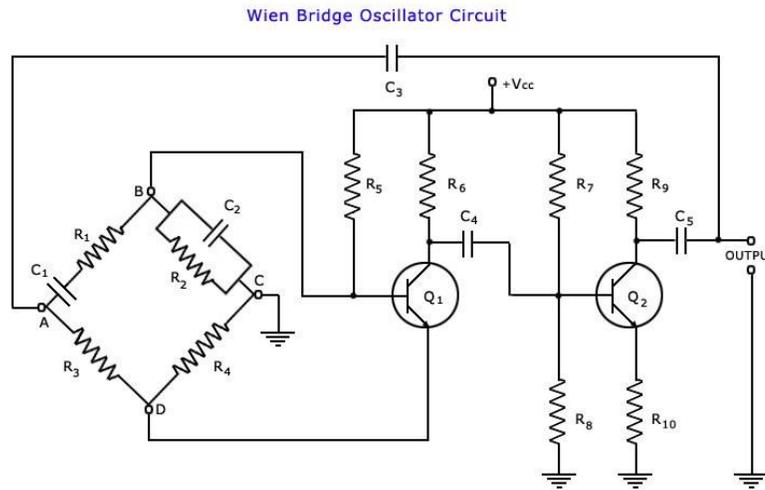
Thus

$$|A| \geq 29$$

## 1.15.2 Wien Bridge Oscillator

### Construction

It is one of the most popular type of oscillator used in audio frequency range. This type of oscillator is simple in design, compact in size, and remarkable stable in its frequency output. Furthermore, its output is relatively free from distortion and its frequency can be varied easily. Frequency output of typical Wien bridge oscillator is only about 1MHz. Lead Lag network produce signal of 0° phase shift, which satisfy the Barkhausen criterion.



**Figure 1.27 Wien Bridge Oscillator**

Feedback ratio of lead lag network is  $1/3$ . Hence to satisfy the condition of unity loop gain, gain of amplifier must be at least 3. To achieve the required gain we can use two common emitter transistor amplifier or an operational amplifier in non-inverting mode.

### Working

As shown in the figure 1.27, it is a two stage amplifier with an RC bridge circuit. By adding Wien bridge feedback network, the oscillator becomes sensitive to a signal of only one particular frequency. This particular frequency is that at which Wien bridge is balanced and for which the phase shift is  $0^\circ$ . The feedback network is employed in the circuit to increase frequency stability. When we switch on the  $+V_{cc}$  supply, a resonating current of frequency  $\frac{1}{2\pi RC}$  flows in the bridge circuit. The current is amplified to achieve the Barkhausen criterion. Since transistor amplifier in CE mode gives  $180^\circ$  phase shift, and the phase shift of bridge circuit is  $0^\circ$ , hence to feedback positive signal to bridge circuit  $180^\circ$  phase shift is required which is provided by another transistor in CE mode. And finally we get sinusoidal signal of stable frequency.

Frequency of oscillation can also be determined by the bridge circuit of oscillator. Bridge is balanced only when

$$R_3 \left[ \frac{R_2}{1 + j\omega C_2 R_2} \right] = R_4 \left[ R_1 - \frac{j}{\omega C_1} \right]$$

$$R_2 R_3 = R_4 (1 + j\omega C_2 R_2) \left( R_1 - \frac{j}{\omega C_1} \right)$$

$$R_2 R_3 = R_4 R_1 - \frac{jR_4}{\omega C_1} + j\omega C_2 R_2 R_1 R_4 + \frac{C_2}{C_1} R_2 R_4$$

$$R_2 R_3 - R_4 R_1 - \frac{C_2}{C_1} R_2 R_4 + \frac{jR_4}{\omega C_1} - j\omega C_2 R_2 R_1 R_4 = 0$$

Separating real and imaginary parts

$$R_2 R_3 - R_4 R_1 - \frac{C_2}{C_1} R_2 R_4 = 0$$

Which gives  $\frac{R_3}{R_4} = \frac{C_2}{C_1} + \frac{R_1}{R_2}$

If  $R_1 = R_2 = R$  and  $C_1 = C_2 = C$  then

$$\boxed{R_3 = 2R_4}$$

And  $\frac{R_4}{\omega C_1} - \omega C_2 R_2 R_1 R_4 = 0$

$$\omega^2 = \frac{1}{C_1 C_2 R_1 R_2}$$

$$\omega = \frac{1}{\sqrt{C_1 C_2 R_1 R_2}}$$

$$f = \frac{1}{2\pi \sqrt{C_1 C_2 R_1 R_2}}$$

If  $R_1 = R_2 = R$  and  $C_1 = C_2 = C$  then

$$\boxed{f = \frac{1}{2\pi RC}}$$

## 1.16 Crystal Oscillator

Most communications and digital applications require the use of oscillators with extremely stable output. Crystal oscillators are invented to overcome the output

fluctuation experienced by conventional oscillators. Some crystals found in nature exhibit the piezoelectric effect. When an ac voltage is applied across them, they vibrate at the frequency of the applied voltage. Conversely, if they are mechanically pressed, they generate an ac voltage. The main substances that produce this piezoelectric effect are Quartz, Rochelle salts, and Tourmaline.

**Rochelle salts** have greatest piezoelectric activity, for a given ac voltage, they vibrate more than quartz or tourmaline. They are used in microphones, headsets and loudspeakers.

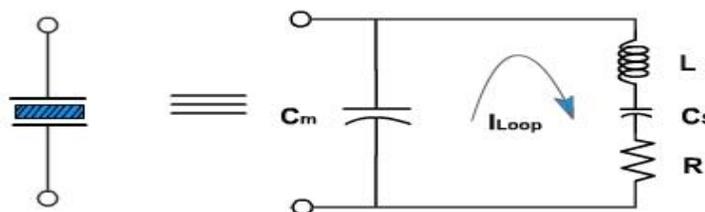
**Tourmaline** shows the least piezoelectric activity but is a strongest of the three. It is most expensive and used at very high frequencies.

**Quartz** is a compromise between the piezoelectric activity of Rochelle salts and the strength of tourmaline. It is inexpensive and easily available in nature. It is most widely used for RF oscillators and filters.

The natural shape of a quartz crystal is a hexagonal prism with pyramids at the ends. To get a useable crystal out of this it is sliced in a rectangular slab form of thickness  $t$ . For use in electronic circuits, the slab is mounted between two metal plates. The fundamental frequency of a crystal is given by

$$f = \frac{1}{t} \quad \text{where } t \text{ is thickness of crystal.}$$

### 1.16.1 AC Equivalent Circuit of Crystal



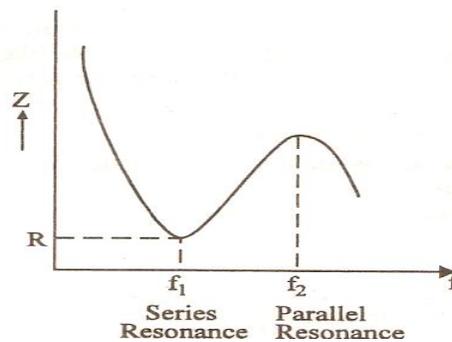
**Figure 1.28 AC Equivalent Circuit of Crystal**

When the mounted crystal is not vibrating, it is equivalent to a capacitance  $C_m$ , because it has two metal plates separated by dielectric,  $C_m$  is known as mounting capacitance. When the crystal is vibrating, it acts like a tuned circuit. Figure shows the ac equivalent circuit of a crystal vibrating at or near its fundamental frequency. Typical values are  $L$  is henrys,  $C_s$  in fractions of a Pico farad,  $R$  in hundreds of ohms and  $C_m$  in Pico farads. The  $Q$  of the

circuit is very high, compared with L-C tank circuit. Because of very high Q, a crystal leads to oscillators with very stable frequency values.

The crystal can have two resonant frequencies as shown in figure 1.29.

- (i) series resonance frequency
- (ii) parallel resonance (or anti-resonance) frequency



**Figure 1.29 Resonant frequency**

**Series resonance frequency**  $f_1$  occurs when  $X_L = X_C$ . At this frequency, crystal offers very low impedance to the external circuit where  $Z = R$ . it is given by:

$$f_1 = \frac{1}{2\pi\sqrt{LC_s}}$$

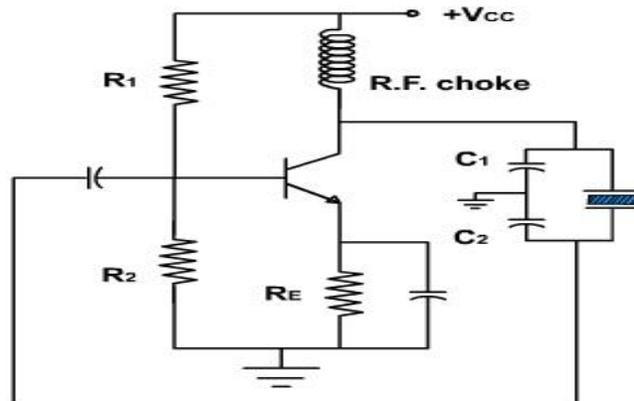
**Parallel resonance (or anti-resonance) frequency**  $f_2$  occurs when reactance of the series leg equals the reactance of  $C_m$ . At this frequency, crystal offers very high impedance to the external circuit. It is given by

$$f_2 = \frac{1}{2\pi\sqrt{LC_p}}$$

Where  $C_p = \frac{C_m C_s}{C_m + C_s}$

### 1.16.2 Pierce Crystal Oscillator

The Colpitts oscillator can be modified by using the crystal to behave as an inductor. The circuit is called Pierce crystal oscillator. The crystal behaves as an inductor for a frequency slightly higher than the series resonance frequency. As only inductor gets replaced by the crystal, which behaves as an inductor, the basic working principle of Pierce crystal oscillator is same as that of Colpitts oscillator.



**Figure 1.30 Pierce Crystal Oscillator**

As shown in figure 1.30, Resistors  $R_1$ ,  $R_2$ , and  $R_E$  provide a voltage-divider stabilized dc bias circuit. Capacitor  $C_E$  provides ac bypass of the emitter resistor to avoid degeneration. The RFC coil provides dc collector load and also prevents any ac signal entering from the dc supply. The coupling capacitor  $C_c$  has negligible reactance at circuit operating frequency but blocks any dc flow between collector and base. The resulting frequency is set by the series resonant frequency of the crystal. Crystal oscillator provides good frequency stability, and there no effect of change in supply voltage, temperature transistor parameters etc.

### Tutorials

1. In the Hartley oscillator  $L_2 = 0.4\text{mH}$  and  $C = .004\mu\text{F}$ . If the frequency of oscillation is 120kHz, find the value of  $L_1$ . Neglect the value of mutual inductance. (***.04mH***)
2. In a transistorized Hartley oscillator, the two inductors are 2mH and 20 $\mu\text{H}$ , while frequency is to be changed from 950kHz to 2050kHz. Calculate the range over which capacitor is to be varied. (***2.98pF – 13.89pF***)
3. In a Hartley oscillator, the value of capacitor in the tuned circuit is 500pF and the two section of coil have inductances 12 $\mu\text{H}$  and 38 $\mu\text{H}$ . Find the frequency of oscillation and the feedback factor  $\beta$ . (***1MHz, .316***)
4. In a Hartley oscillator,  $L_2 = 15\text{mH}$  and  $C = 50\text{pF}$ . Calculate  $L_1$  for a frequency of 168kHz. The mutual inductance between  $L_1$  and  $L_2$  is 5 $\mu\text{H}$ . Also find the required feedback factor for the oscillation. (***2.945mH, 0.196***)
5. In the Colpitts oscillator,  $C_1 = 0.2\mu\text{F}$  and  $C_2 = 0.02\mu\text{F}$ . If the frequency of oscillation is 10kHz, find the value of the inductor. Also find the required feedback for oscillation. (***13.932mH, 0.1***)

6. A Colpitts oscillator is designed with  $C_2 = 100\text{pF}$  and  $C_1 = 7500\text{pF}$ . The inductance is variable. Determine the range of inductor the frequency of oscillation is to vary between 950kHz to 2050kHz. **(61 $\mu\text{H}$ -284 $\mu\text{H}$ )**
7. In an RC phase shift oscillator, if  $R_1 = R_2 = R_3 = 200\text{k}\Omega$  and  $C_1 = C_2 = C_3 = 100\text{pF}$ . Find the frequency of oscillation **(3.248kHz)**
8. In an RC phase shift oscillator, if its frequency of oscillation is 955Hz and  $R_1 = R_2 = R_3 = 680\text{k}\Omega$ , find the value of capacitor used. **(100pF)**
9. In a Wien bridge oscillator, if the value of R is 100k $\Omega$ , and frequency of oscillation is 10kHz. Find the value of capacitor. **(159pF)**
10. The frequency sensitive arm of the Wien bridge oscillator uses  $C_1 = C_2 = 0.001\mu\text{F}$  and  $R_1 = 10\text{k}\Omega$  while  $R_2$  is kept variable. The frequency is to be varied from 10kHz to 50kHz, by varying  $R_2$ . Find the minimum and maximum value of  $R_2$ . **(1.013k $\Omega$ , 25.33k $\Omega$ )**
11. A crystal has following parameters:-  $L = 0.4\text{H}$ ,  $C = 0.085\text{pF}$  and  $C_m = 1\text{pF}$  with  $R = 5\text{k}\Omega$ . find
  - (i) Series resonant frequency
  - (ii) Parallel resonant frequency
  - (iii) Q factor of coil. **(856kHz, 899kHz, 430.27)**
12. A crystal has  $L = 2\text{H}$ ,  $C = 0.01\text{pF}$ , and  $R = 2\text{k}\Omega$ . Its mounting capacitance is 2pF. calculate its series and parallel resonating frequency. **(1.125MHz, 1.128MHz)**